

Week 14: Beam Buckling

- Euler Buckling
- Effective length for buckling
- Effect of eccentricity

Stability- different criteria for resisting loads



Strength: the ability of a structure to withstand a load without the development of excessive stress

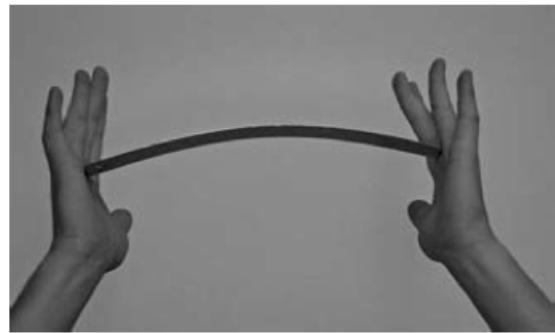
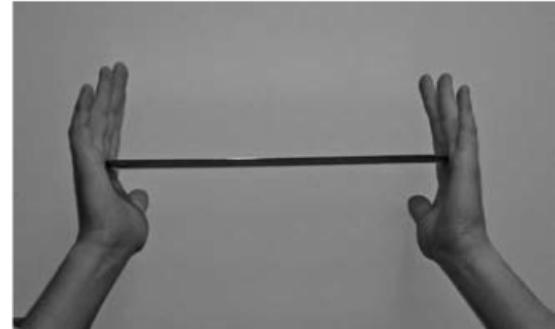


Stiffness: the ability of a structure to withstand a load without developing excessive deformation.

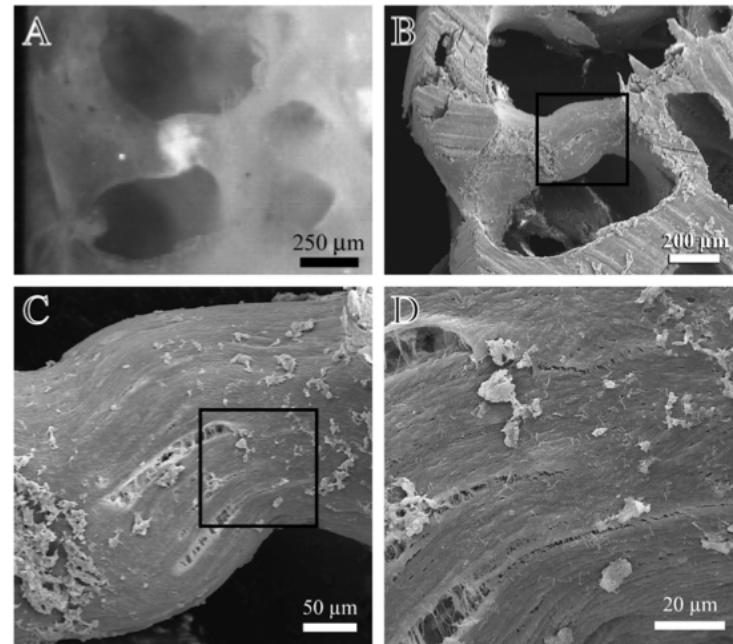
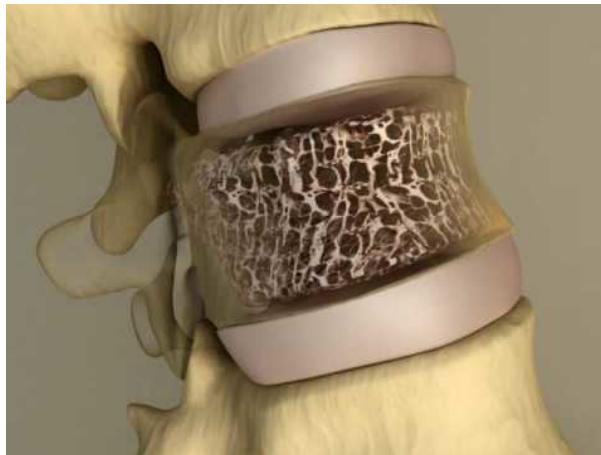


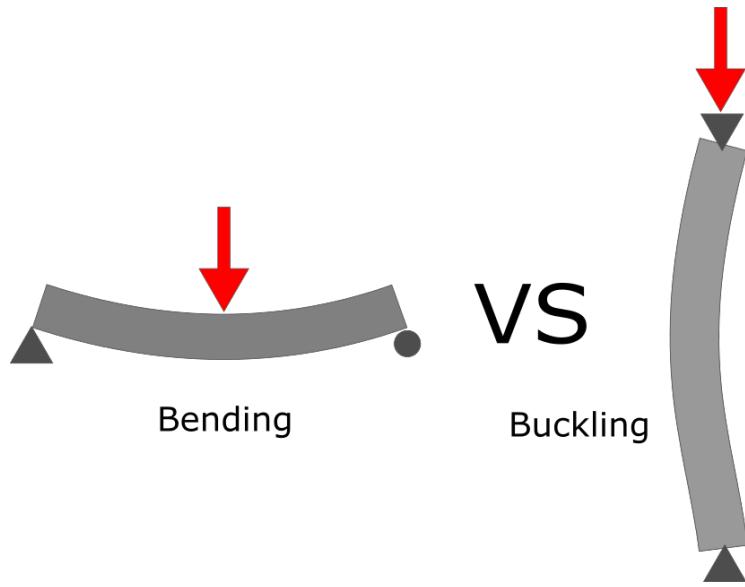
Stability: the ability of a structure to withstand a load without experiencing a sudden change in configuration

Buckling



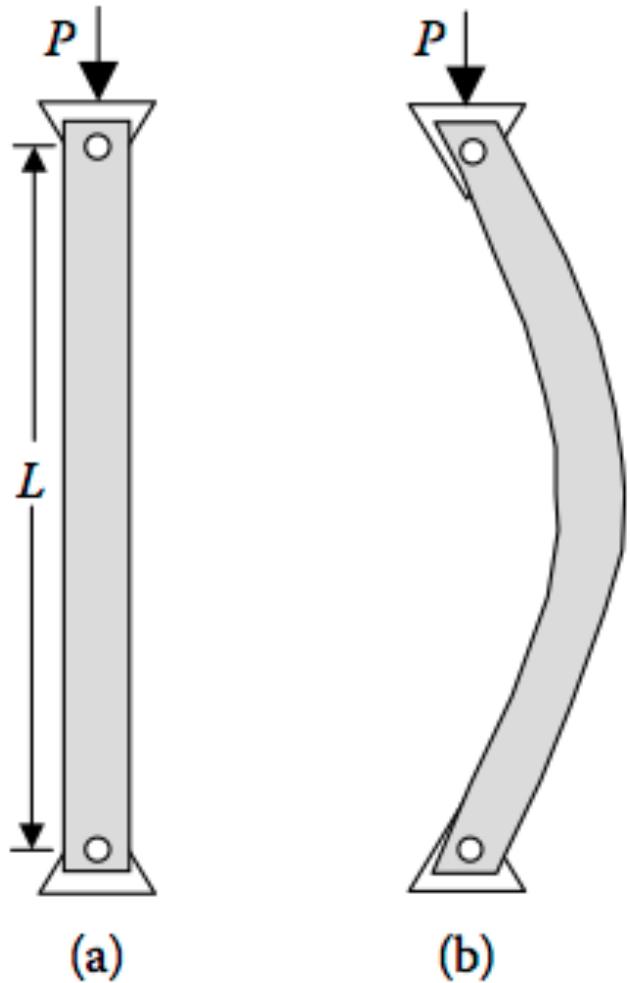
Buckling is important from the macro to the microscale





Buckling

- Buckling is a type of instability that occurs when a beam fails under a compressive load much smaller than the load necessary to reach the yield stress
- In buckling, the failure occurs because the applied load results in a sudden deformation in a perpendicular direction.

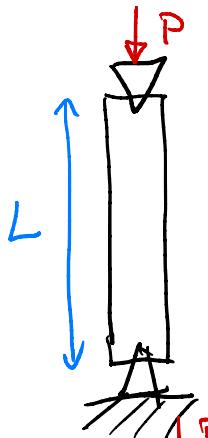


Euler Buckling

Two regimes of deformation when a beam is loaded in compression:

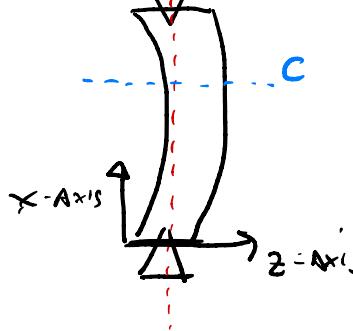
1. If the axial load on a beam is small, the change in length will be due to compressive strain. $P < P_{cr}$
2. If the axial load on a beam P is larger than the critical load P_{cr} , then the beam becomes unstable and a small perturbation will result in buckling of the beam.

Euler Buckling:

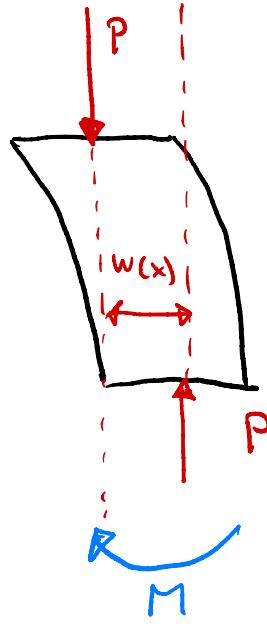


$$\square P < P_{CR} \Rightarrow \Delta L = L \cdot \varepsilon = L E \frac{P}{A}$$

$$\square P > P_{CR} \Rightarrow \text{Buckling}$$



\Rightarrow TAKE VIRTUAL SECTION THROUGH
BEAM AT HEIGHT C



- DUE TO BENDING OF BEAM: THE LOAD P IS NO LONGER CO-LINEAR WITH THE REACTION LOAD ON THE VIRTUAL SECTION
 - ⇒ AN INTERNAL MOMENT MUST EXIST THAT KEEPS THE SECTION FROM ROTATING

□ INTERNAL MOMENT: $M(x) = P \cdot w(x)$

□ WE KNOW FROM BEAM BENDING:

$$\frac{d^2 w}{dx^2} = - \frac{M}{EI} = - \frac{P}{EI} w(x)$$

□ DIFF. EQN. FOR BUCKLING:

$$\frac{d^2 w}{dx^2} + \frac{P}{EI} w = 0$$

- Solving with characteristic polynomials:

$$\lambda^2 + \frac{P}{EI} = 0 \Rightarrow \lambda = \pm i \sqrt{\frac{P}{EI}}$$

- TME solution with: $\lambda = \alpha \pm bi$ $b = \sqrt{\frac{P}{EI}}$ $a = 0$

$$w(x) = e^{\alpha x} (c_1 \cos bx + c_2 \sin bx)$$

$$\underline{w(x) = c_1 \cos \sqrt{\frac{P}{EI}} x + c_2 \sin \sqrt{\frac{P}{EI}} x}$$

- c_1 & c_2 through B.C.

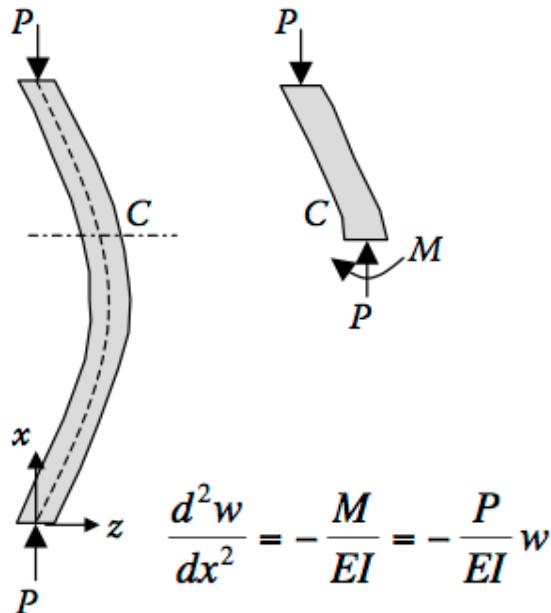
$$w(0) = 0 \Rightarrow c_1 = 0$$

$$w(L) = 0 \Rightarrow c_2 \sin \left(\sqrt{\frac{P}{EI}} L \right) = 0$$

$$\sin \left(\sqrt{\frac{P}{EI}} L \right) = 0$$

$$\sqrt{\frac{P}{EI}} L = n \cdot \pi \quad n \in \mathbb{Z}$$

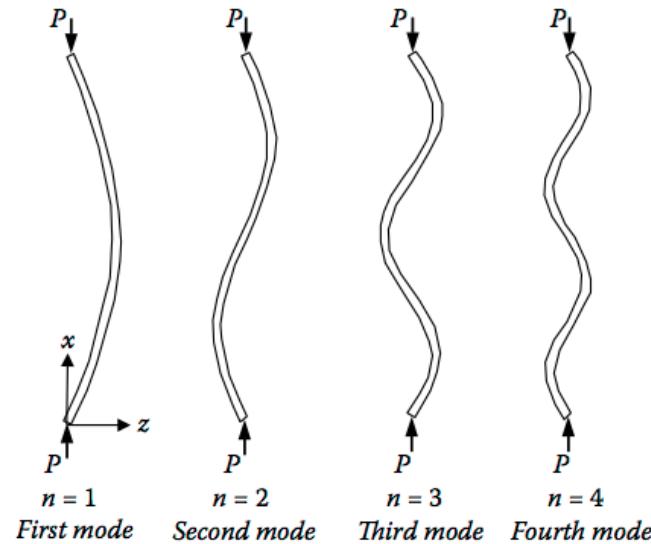
$$P = \frac{n^2 \pi^2}{L^2} EI$$



$$\frac{d^2w}{dx^2} + \frac{P}{EI}w = 0$$

Euler Buckling

We can derive the Euler Buckling formula using the method of sections through the buckled beam.



Euler Buckling

The differential equation has multiple solutions:

This results in multiple buckling modes:

$$P = \frac{n^2 \pi^2 EI}{L^2}$$

- For the critical buckling load we get then *Euler's Buckling Formula*:

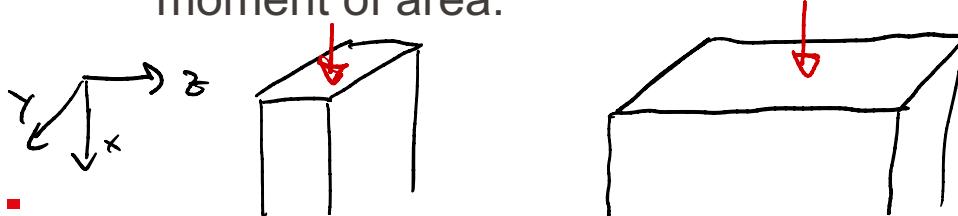
$$P_{cr} = \frac{\pi^2 EI}{L^2}.$$

- With the shape of the buckled beam:

$$w(x) = a \sin\left(\frac{\pi}{L}x\right)$$

$$\begin{aligned} w(x) &= c_2 \sin\left(\sqrt{\frac{P_{cr}}{EI}} x\right) \\ &= c_2 \sin\left(\frac{\pi}{L} x\right) \end{aligned}$$

- The second moment of area (I) should be taken around the axis around which the beam buckles. This is in general the axis with the smallest second moment of area.



$$P_{cr} = \frac{\pi^2 EI}{L_e^2}$$

Effective Length L_e as Function of Supports

End Conditions	Effective Length
Fixed-Free	$Le = 2L$
Pinned-Pinned	$Le = L$
Fixed-Pinned	$Le = 0.7L$
Fixed-Fixed	$Le = 0.5L$

Euler Buckling : Effective length

- The Euler Formula we have derived here only deals with a beam with pinned supports on each end.
- The type of support however greatly influences the critical load and the buckling behavior.
- Euler's formula can be extended towards other types of support by using the concept of the effective length.

- Critical buckling stress:

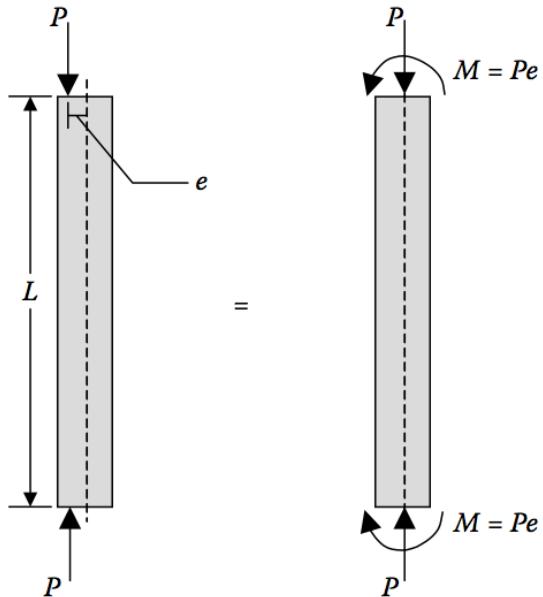
$$\sigma_{cr} = \frac{P_{cr}}{A} = \frac{\pi^2 EI}{L_e^2 A}$$

- Using the definition of the radius of gyration $r = \sqrt{\frac{I}{A}}$:

$$\sigma_{cr} = \frac{\pi^2 E A r^2}{L_e^2 A} = \frac{\pi^2 E r^2}{L_e^2} = \frac{\pi^2 E}{(L_e / r)^2}$$

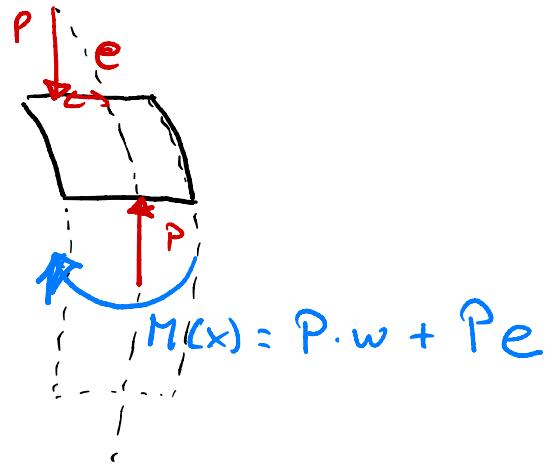
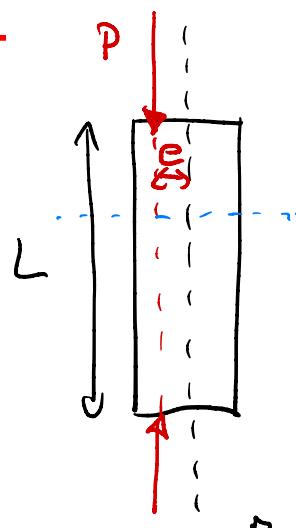
- L_e/r is the slenderness ratio

$$w(x) = c_2 \sin\left(\frac{\pi}{L} x\right)$$



Buckling: Effect of eccentricity

- So far, we've looked at beams that were loaded through the centroid of the column
- Often, the load is offset from this axis: eccentric loading
- We calculate the behavior of a beam pinned at both ends with eccentric load.
- We can model the eccentricity with an axial load and a moment at the supports



$$\frac{d^2 w}{dx^2} = -\frac{M}{EI} = -\frac{P}{EI} w - \frac{P}{EI} e$$

□ Inhomogeneous differential eqn:

$$\boxed{\frac{d^2 w}{dx^2} + \frac{P}{EI} w = -\frac{P}{EI} e}$$

□ Solve through Ansatz: $w(x) = a$

$$\frac{Pa}{EI} = -\frac{P}{EI} e \Rightarrow a = -e$$

□ General solution of this inhomogeneous Eqn is :

$$w(x) = c_1 \cos\left(\sqrt{\frac{p}{EI}} x\right) + c_2 \sin\left(\sqrt{\frac{p}{EI}} x\right) - e$$

□ BC:

$$w(0) = 0 \Rightarrow c_1 = e$$

$$w(L) = 0 \quad -e \cos\left(\sqrt{\frac{p}{EI}} \cdot L\right) + c_2 \sin\left(\sqrt{\frac{p}{EI}} \cdot L\right) - e = 0$$

with trigonom. formulas: $\frac{1 - \cos x}{\sin x} = \tan \frac{x}{2}$

$$c_2 = e \tan\left(\sqrt{\frac{p}{EI}} \cdot \frac{L}{2}\right)$$

⇒ FORMULAS FOR DEFLECTION IN BUCKLING:

$$w(x) = e \cos \left(\sqrt{\frac{P}{EI}} x \right) + e \tan \left(\sqrt{\frac{P}{EI}} \frac{L}{2} \right) \cdot \sin \left(\sqrt{\frac{P}{EI}} x \right) - e$$

□ MAXIMUM DEFLECTION is AT $x = \frac{L}{2}$ FOR $P < P_{CR}$

$$w_{MAX} = e \left\{ \sec \left(\sqrt{\frac{P}{EI}} \frac{L}{2} \right) - 1 \right\} \quad \sec = \frac{1}{\cos}$$

□ Buckling occurs AT P_{CR} with $w = \infty$

$$\sec \left(\frac{\pi}{2} \right) = \infty \Rightarrow \sqrt{\frac{P_{CR}}{EI}} \cdot \frac{L}{2} = \frac{\pi}{2}$$

$$\Rightarrow P_{CR} = \frac{\pi^2 EI}{L^2}$$

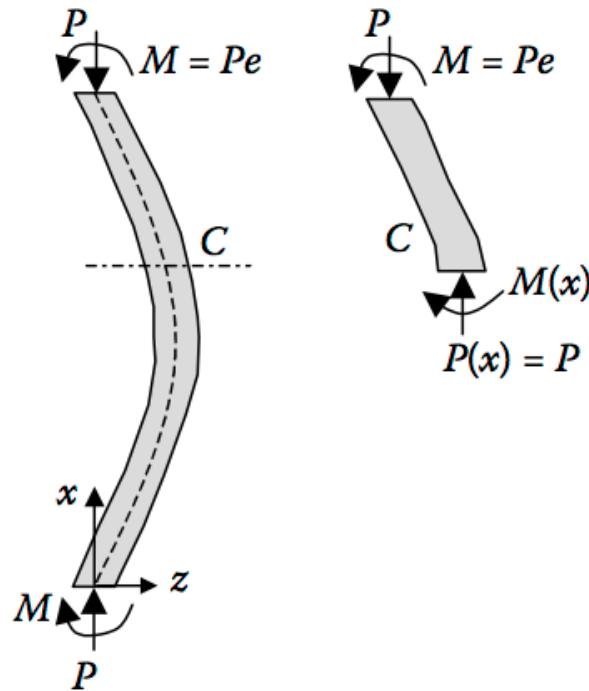
Critical Load

■ Maximum stress in column before buckling: $\sigma_{\text{comp}} + \sigma_{\text{bending}}$

$$\sigma_{\text{MAX}} = -\frac{P}{A} \left\{ 1 - \frac{c \cdot c}{r^2} \sec \left(\sqrt{\frac{P}{EI}} \frac{L}{2} \right) \right\}$$

$$r = \sqrt{\frac{I}{A}}$$

c = maximum distance
from centroid
to surface



Buckling: Effect of eccentricity

- Centric load: P
- Moment: $M = P^*e$
- This means that the beam bends even under small loads without the beam buckling
- We solve the now inhomogeneous differential equation:

$$\frac{d^2w}{dx^2} + \frac{P}{EI}w = -\frac{P}{EI} \cdot e$$

- For the deflection we then get:

$$w(x) = e \left\{ \tan \left(\sqrt{\frac{P}{EI}} \cdot \frac{L}{2} \right) \cdot \sin \left(\sqrt{\frac{P}{EI}} \cdot x \right) + \cos \left(\sqrt{\frac{P}{EI}} \cdot x \right) - 1 \right\}$$

- And for the maximum deflection:

$$w_{max} = w(L/2) = e \left[\sec \left(\sqrt{\frac{P}{EI}} \frac{L}{2} \right) - 1 \right]$$

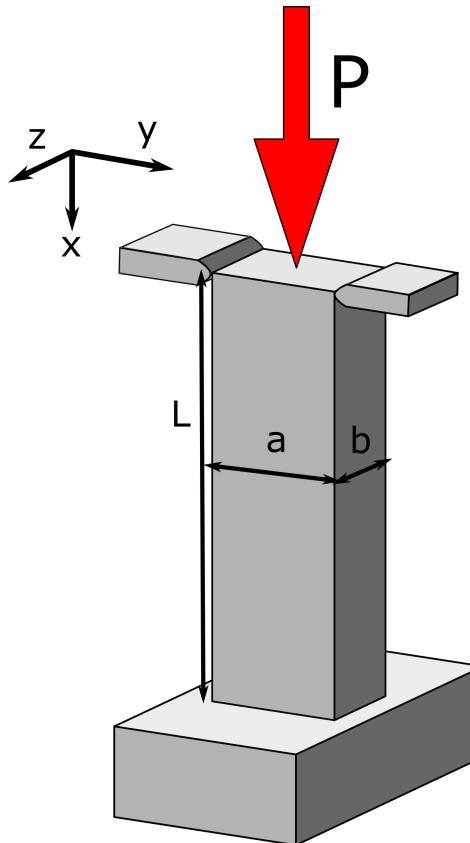
- The critical buckling load is then

$$P_{cr} = \frac{\pi^2 EI}{L^2}$$

- Maximum stress in the beam is given by the compressive stress and the bending stress:

$$\sigma_{max} = -\frac{P}{A} \left[1 - \frac{ec}{r^2} \sec \left(\sqrt{\frac{P}{EI}} \frac{L}{2} \right) \right]$$

$$\sigma_{max} = -\frac{P}{A} \left[1 - \frac{ec}{r^2} \sec \left(\sqrt{\frac{P}{P_{cr}}} \frac{\pi}{2} \right) \right]$$

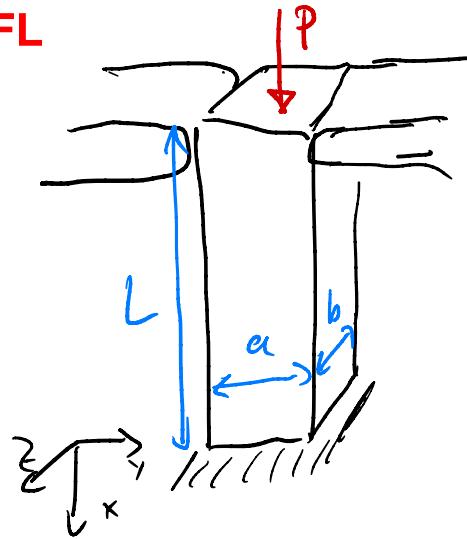


Example Buckling

An aluminum column of length L and rectangular cross section has a fixed end B and supports a centric axial load at A .

Two smooth and rounded fixed plates restrain end A from moving in one of the vertical planes of symmetry but allow it to move in the other plane.

- Determine the ratio a/b of the two sides of the cross section corresponding to the most efficient design against buckling.
- Design the most efficient cross section for the column, knowing that $L = 50$ cm, $E = 70$ GPa, $P = 22$ kN and that a safety factor of 2.5 is required.



- GIVEN:
- GEOMETRY: $L = 50 \text{ cm}$
 - LOADS: $P = 22 \text{ kN}$
 - MAT PROP: $E = 70 \text{ GPa}$
 - SAFETY FACT: 2.5

- ASKED:
- a/b FOR LARGEST $P_{\text{crit}}^{\text{tors}}$ @ $A = a \cdot b$
 - A_{\min} TO WITHSTAND $P = 22 \text{ kN}$ @ $SF = 2.5$
- APPROACH: Buckling with different B.C.

■ ANSWER:

- Buckling possible in xy & xz planes
- xy & xz have different supports

xy : FIXED - PINNED SUPPORT

xz : FIXED - FREE

□ Most efficient design: $P_{CR}^{\text{xy}} = P_{CR}^{\text{xz}}$

$$P_{CR} = \frac{\frac{\pi^2 E I}{L_e^2}}{I}$$

$$P_{CR}^{\text{xy}} = \frac{\frac{\pi^2 E I_z}{(L_e^{\text{xy}})^2}}{I} = \frac{\frac{\pi^2 E I_z}{(L_e^{\text{xz}})^2}}{I} = P_{CR}^{\text{xz}}$$

$$I_z = \frac{b a^3}{12}$$

$$L_e^{\text{xy}} = 0,7L \dots \text{fixed-pinned}$$

$$\frac{\frac{\pi^2 E I_z}{(0,7)^2}}{I} = \frac{\pi^2 E I_z}{2^2} \Rightarrow \frac{a^2}{b^2} = \frac{0,7^2}{4} \Rightarrow \boxed{\frac{a}{b} = 0,35} \Rightarrow a = 0,35 \cdot b$$

$$I_z = \frac{ab^3}{12}$$

$$L_e^{\text{xz}} = 2L \dots \text{fixed-free}$$

ANSWER TO PART b:

$$P_{cr} = 2.5 \cdot P = 55 \text{ kN}$$

$$P_{cr} = \frac{\pi^2 EI}{L_e^2}$$

$$I_y = \frac{ab^3}{12} \quad a = 0.35b$$

$$L_e = 2L \quad E = 70 \text{ GPa}$$

$$= \frac{\pi^2 E}{2} \cdot \frac{ab^3}{12} = 55 \text{ kN}$$

$$= \frac{\pi^2 E}{48L^2} \cdot 0.35b^4 = 55 \text{ kN}$$

$$\Rightarrow b^4 = \frac{48L}{0.35 \cdot \pi^2 E} \cdot 55 \text{ kN}$$

$$\Rightarrow b = 4.06 \text{ cm} \Rightarrow \underline{\underline{4.1 \text{ cm}}}$$

$$\underline{\underline{a = 1.4 \text{ cm}}}$$